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The Steric Repulsion Properties of Polyethylene Oxide

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Polyethylene oxide (PEO) surfaces are recognized as having an effective steric stabilization character. A theoretical scaling analysis involves the osmotic and elastic coefficients of the polymer as a function of molecular weight, in a good solvent. The calculated results show that PEO in water may exhibit the greatest flexibility among water soluble polymers, probably due to its lowest elastic contribution.

Introduction

Polymers adsorbed on solid surfaces immersed in a liquid medium are considerably protected against aggregation, a phenomenon termed steric stabilization. There exist long-range repulsion forces between two surfaces bearing such adsorbed layers, and these repulsive forces overcome the attractive van der Waals forces acting between the bare surfaces.

Polyethylene oxide (PEO) adsorbed surfaces are recognized as effective in minimizing protein adsorption¹⁻⁵, probably due to a steric stabilization effect^{6,7}. Direct force measurements⁸⁻¹⁰ between two adsorbed PEO surfaces onto mica in a good aqueous 0.1 M KNO₃ solvent by the Israelachvili force method¹¹ show that the repulsion forces develop at certain separation distances due to the steric repulsion phenomenon.

A scaling model of chains adsorbed onto a surface in a good solvent was proposed by Alexander¹² and further extended by de Gennes¹³ to give a form for the steric repulsion force profile. The force is analyzed in terms of a repulsive

osmotic term, which comes from the increased polymer concentration in the intersurface gap as the surfaces approach, and an elastic term in which the reduction in free energy, on compression of the over-extended chains, is taken into account. The Alexander-de Gennes model has been developed into a theory of the forces between two such adsorbed layers by Patel *et al.*¹⁴. Their result is that the force *vs* separation distance between two adsorbed surfaces can be expressed as a universal dimensionless function which contains two unknown proportionality constants resulting from the osmotic and elastic contributions.

In this paper, the more effective character of PEO for protein-resistant surfaces was studied by comparison of the osmotic and elastic coefficients of PEO of several molecular weights in good aqueous electrolyte and toluene solvents. The osmotic and elastic coefficients of PEO in aqueous electrolyte and toluene solvents were estimated by the universal curve-fitting method of Patel *et al.*¹⁴ adsorbed on mica surfaces in 0.1 M aqueous KNO₃^{8,9,15,16} and toluene solvents^{10,16,17}, using a least-squares curve fitting method. The data for polystyrene (PS) adsorbed on mica surface in toluene^{7,18} is also

Table 1. The Calculated Osmotic and Elastic Coefficients of PEO and PS in Aqueous 0.1 M KNO₃ and Toluene Solvents with the Variation of Molecular Weight of Polymer

	PEO in aq. KNO ₃		PEO in toluene			PS in toluene		
M_w	3.1×10^5	4.0×10^4	3.1×10^5	1.6×10^5	4.0×10^4	3.75×10^5	1.81×10^5	1.41×10^5
Γ (mg · m ⁻²)	4.0	4.0	2.0	1.5	1.0	3.0	1.6	3.0
L_0 (exp) (Å)	400	225	750	550	280	1100	750	650
k_1	0.004	0.002	0.12	0.23	0.18	0.64	11.44	1.50
k_2	0.12	0.025	1.08	0.68	0.24	0.07	0.75	0.16
L_0 (Å)	397	218	705	640	270	1170	690	616

considered for comparison.

Method

The universal dimensionless function relating the dimensionless energy (ϵ) and dimensionless separation distance (∂) in a good solvent was obtained by Patel *et al.*¹⁴ as follows:

$$\epsilon = 4\pi k_1 x^{5/4} \{[(x\partial)^{-5/4} - 1] + (5/7)[(x\partial)^{7/4} - 1]\} \quad (1)$$

where,

$$x^3 = (7/5)(k_2/k_1), \quad \partial = D/(2aN\sigma^{1/3}),$$

and

$$\epsilon = (F/R)(a^2/k_B T)(1/N\sigma^{11/6})$$

In these formulas, two unknown proportionality coefficients, k_1 and k_2 , are referred to as the osmotic and elastic contributions to the force, respectively, D is the separation distance between the two adsorbed surfaces, a is the size of a segment of the polymer chain (2.78 Å for PEO and 2.22 Å for PS from crystallographic data¹⁹⁻²¹), N is the number of segments in the nonadsorbing part of the chain, $k_B T$ is the thermal energy, F/R is the force between crossed cylinders having radius R , which is 2π times the energy per unit area of interaction between parallel plates²², and σ is a dimensionless surface density of chains emanating from the surface, $\sigma = a^2/\delta^2$, where δ is the average spacing between chains on the surface.

The surface density (σ) can be calculated from the data of adsorbed amounts by assuming hexagonal packing of spheres of polymer¹⁵. D and F/R are given by the published experimentally determined force *vs* separation distance plots, which are reduced to the dimensionless distance (∂) and dimensionless energy (ϵ) based on σ . The coefficients k_1 and x are then calculated from Eq. (1) by using the least-squares curve fitting method, giving the final k_1 and k_2 values for PEO and PS of several molecular weights in good aqueous electrolyte and toluene solvents.

Force *vs* separation profiles^{7-10,15-18} represent the onset of repulsions as a function of separation distance, which is the basis of the experimentally determined effective layer thickness of the adsorbed chains, L_0 (exp), as measured by half the range for onset of repulsive interactions. The theoretically effective single layer thickness of the adsorbed chains, L_0 , is given by consideration of the osmotic and elastic contributions, $L_0 = [(5/7) \cdot (k_1/k_2)]^{1/3} \cdot Na\sigma^{1/3}$, which is also compared with the L_0 (exp).

Results and Discussion

The calculated results from the published data^{7-10,15-18} are given in Table 1. To some extent, a consistency of experimental and theoretical layer thickness values of adsorbed chains (L_0 (exp) and L_0) tells that the theory is about correct and suitable to study the steric repulsion properties of PEO in water. The remaining data except L_0 are inconsistent and are not easily comparable with each other, which may be largely due to the lack of certainties of experimentally determined adsorbed amounts (the adsorbed amounts affect the degree of osmotic and elastic contributions to the force). The adsorbed amounts in the literature are rough values, which is verified by the experimental fact^{8,9,15,16} that all direct force measurements between two adsorbed polymer surfaces show different force values, even for measurements at the same molecular weight and solvent conditions, i.e., different measurements for the same sample produce the different results (in part due to difference in the adsorbed amounts of polymer on the surface).

The repulsive osmotic coefficient is increased due to increased polymer concentration in the intersurface gap as the surfaces approach. The osmotic effect will dominate at very high compressions^{7,15} and is expressed in Eq. (1). If Table 1 is looked at as a rough estimate, the osmotic coefficients (k_1) are nearly similar for each different polymer-solvent system in spite of the difference of molecular weight, which means that the osmotic pressure is about the same for the same polymer-solvent systems. The comparison of k_1 values for each different polymer-solvent system (about >1 for PS-toluene, 0.1-0.5 for PEO-toluene, and 0.002-0.01 for PEO-aqueous KNO₃) show that toluene is a good solvent for PS and PEO and the aqueous 0.1 M KNO₃ solution is a solvent (not good) for PEO. Toluene is a better solvent for PS than PEO, which is also supported by the experimental fact that the PEO block is adsorbed onto the mica and PS does not, for PS-PEO diblock copolymers in toluene¹⁷. To have approximately the same value of k_1 for different molecular weight PEO-water systems, it is necessary to control the adsorbed amounts. It is also a prior condition that the adsorbed amounts generally increase with adsorption of longer chains¹⁰. The same procedures are also applied for PEO-toluene and PS-toluene systems. The results are shown in Table 2. Comparing the L_0 values, PEO is less stretched in aqueous 0.1 M KNO₃ solvent than in toluene, which could be due in part to a greater decrease in k_1 in aqueous solvent. The lower value of k_1 of PEO in aqueous electrolyte than in orga-

Table 2. The Revised Osmotic and Elastic Coefficients of PEO and PS in Good Solvents with the Correction of the Adsorbance

	PEO in aq. KNO ₃		PEO in toluene			PS in toluene		
M_w	3.1×10^5	4.0×10^4	3.1×10^5	1.6×10^5	4.0×10^4	3.75×10^5	1.8×10^5	1.41×10^5
Γ (mg · m ⁻²)	4.0	3.2	1.6	1.6	0.9	2.1	3.9	3.0
k_1	0.004	0.004	0.2	0.2	0.2	1.5	1.5	1.5
k_2	0.12	0.03	1.43	0.51	0.23	0.12	0.25	0.16
L_0/L_c (%)	3.95	8.6	3.6	6.3	10.7	14.6	17.9	20.5

nic solvent is also supported by the polymer-solvent interaction parameter, χ (0.39 and 0.48 for PEO-toluene²³ and PEO-0.1 M KNO₃²⁴, respectively). Values of χ up to 0.5 are found for systems showing complete miscibility, while for $\chi > 0.5$ the systems are characterized by only limited miscibility, with higher values of χ corresponding to decreasing extent of interaction of the two components⁴. In our previous study²⁵, the osmotic contribution has the more effect on the chain extension than the elastic contribution. The variation of the k_1 value has the more effect on the change of the layer thickness of the chain in a good solvent.

The effects of k_1 and k_2 values on the steric force are opposite; the increase of osmotic contribution (k_1) gives rise to an increase of the spacing between chains in solvent, stretching them. On the other hand the elastic contribution (k_2) is a stiffness factor; its increase makes the chain more stiff and less flexible, and harder to stretch. PEO in water has lower k_1 and k_2 values than in other solvent systems. The lower the k_1 value, the less stretch (i.e., it is less effective for steric repulsion) of the chain. On the other hand, the lower the k_2 value, the more flexible the chain. The k_2 value of PEO in aqueous solvent is lower than in any other investigated polymer-solvent systems.

PEO is very flexible and movable. Long flexible PEO chains on the surface have been called "molecular cilia" by Nagaoka and coworkers³. Thus the prominent steric repulsion properties of PEO in water are mainly contributed by this flexibility, which is probably caused by the large decrease in k_2 in spite of the decrease of k_1 . On the other hand, the remarkable stretching of the PS chain in toluene is mainly attributed to the large increase in the osmotic contribution in spite of the increase of the elastic contribution. Table 2 shows that change of molecular weight has great influence on the degree of the elastic contribution to the force and also on the layer thickness (L_0) (the osmotic contribution is assumed to be constant for the same polymer-solvent system, even if the molecular weight of polymer is varied). L_0 can be compared with the fully extended layer thickness (contour length)²⁶, $L_c = aN$. L_0/L_c values are shown in last row of Table 2. The chains are stretched to about 3 to 20% of their fully extended length according to their molecular weight. Considering the effect of solvent on PEO, for a given mass of polymer the L_0/L_c values are similar for each PEO-solvent systems in spite of the larger decrease in k_1 value in aqueous electrolyte, which could be due to a decrease in k_2 value and the difference in the conformation of the PEO in organic solvents and in water. PEO in organic solvents exists as a random coil, whereas in water its conformation is helical^{4,27,28}. As the molecular weight of the polymer

is decreased, the ratio, L_0/L_c , is increased, mainly due to the larger decrease of the elastic contribution. The chain is actually more flexible and stretched, as the chain is shortened. Thus the longest chain of PEO in water without any flexibility may not be effective for steric repulsion, which is supported experimentally³ and theoretically^{24,29} by some investigators. A suitable length of PEO with higher flexibility (higher L_0/L_c value) is appropriate for steric repulsion, i.e., protein-resistance.

Conclusion

We examined the main factors in the prominent steric repulsion properties of PEO adsorbed surfaces in water, considering the osmotic and elastic contributions to the steric repulsion force. As the elastic contribution of the polymer chain in a good solvent is lowered, the stiffness is lowered, and the flexibility is increased. PEO in water has the highest flexibility, probably caused by having the lowest elastic contribution. The prominent steric repulsion properties of PEO adsorbed surfaces in water may be mainly due to the greater contribution of an elastic factor than an osmotic one. Comparing the osmotic contributions of various polymer-solvent systems, water may not be a very good solvent for PEO, and toluene is a good solvent for both PEO and PS, but it is a better one for PS. The layer thickness of the chains is mainly controlled by the osmotic factor, so longer chains are observed in PS-toluene than in any other polymer-solvent system because of higher osmotic contribution to the steric repulsion force. As the molecular weight of the polymer is lowered, the chain is more stretched to its fully extended state and is more flexible. Thus a moderate length of PEO with higher flexibility should be more suitable for steric repulsion.

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Electrical Conductivity of the Solid Solutions X ZrO₂ + (1 - X) Yb₂O₃; 0.01 ≤ X ≤ 0.09

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ZrO₂-doped Yb₂O₃ solid solutions containing 1, 3, 5, 7 and 9 mol% ZrO₂ were synthesized from spectroscopically pure Yb₂O₃ and ZrO₂ powders and found to be rare earth C-type structure by XRD technique. Electrical conductivities were measured as a function of temperatures from 700 to 1050°C and oxygen partial pressures from 1 × 10⁻⁵ to 2 × 10⁻¹ atm. The electrical conductivities depend simply on temperature and the activation energies are determined to be 1.56-1.68 eV. The oxygen partial pressure dependence of the electrical conductivity shows that the conductivity increases with increasing oxygen partial pressure, indicating *p*-type semiconductor. The P_{O₂} dependence of the system is nearly power of 1/4. It is suggested from the linearity of the temperature dependence of electrical conductivity and only one value of 1/*n* that the solid solutions of the system have single conduction mechanism. From these results, it is concluded that the main defects of the system are negatively doubly charged oxygen interstitial in low-ZrO₂ doping level and negatively triply charged cation vacancy in high doping level and the electrical conduction is due to the electronic hole formed by the defect structure.

Introduction

Oxides of the rare-earth elements generally have the rare-earth C-type structure when the ratio of the radius of oxygen anion to that of metal cation is between 0.60 to 0.89¹. And the number of oxygen anions occupied on the lattice sites is six and two of eight lattice oxygen sites become vacancies². Accordingly, the oxides of these rare-earth elements have

similar physical properties. It was reported that Sm₂O₃, Gd₂O₃ and other oxides belonging to these rare-earth C-type oxides have mixed conduction mechanism that ionic conduction occurs predominantly over electronic conduction^{3,4}, whereas in the case of Yb₂O₃, there were few experimental data because of thermal instability.

Kang et al.⁵ reported that above 700°C, pure Yb₂O₃ has the activation energy of from 1.92 to 1.95 eV and shows